U.S. Department of Transportation

Federal Aviation

Administration

Advisory Circular

TAXI, TAKEOFF AND LANDING ROLL DESIGN LOADS

Date: Initiated by: ANM-110 AC No. 25.491-1 Change:

- 1. <u>PURPOSE</u>. This advisory circular (AC) sets forth acceptable methods of compliance with the provisions of part 25 of the Federal Aviation Regulations (FAR) dealing with the certification requirements for taxi, takeoff and landing roll design loads. Guidance information is provided for showing compliance with § 25.491 of the FAR, relating to structural design for airplane operation on paved runways and taxiways normally used in commercial operations. Other methods of compliance with the requirements may be acceptable.
- 2. <u>RELATED FAR SECTIONS</u>. The contents of this AC are considered by the Federal Aviation Administration (FAA) in determining compliance with § 25.491 of the FAR. Related sections are §§ 25.305(c) and 25.235.

3. BACKGROUND.

- a. All paved runways and taxiways have an inherent degree of surface unevenness, or roughness. This is the result of the normal tolerances of engineering standards required for construction, as well as the result of events such as uneven settlement and frost heave. In addition, repair of surfaces on an active runway or taxiway can result in temporary ramped surfaces. Many countries have developed criteria for runway surface roughness. The International Civil Aviation Organization (ICAO) standards are published in ICAO Annex 14.
- b. In the late 1940's, as airplanes became larger, more flexible, and operated at higher ground speeds, consideration of dynamic loads during taxi, landing rollout, and takeoff became important in airplane design. The Civil Aeronautics Administration, in Civil Air Regulations 4b (CAR 4b), § 4b.172, required the effects of landing gear deflection during taxiing over the roughest ground expected in service to be considered relative to its effect on damage to structural components. The CAR 4b, § 4b.235, also required the airplane be designed, in part, to withstand loads calculated under § 4b.172. Those regulations were carried over to part 25 of the FAR as § 25.235 and § 25.491 respectively. Substantiation of the effect of ground loads on flexible structure is required by § 25.305(c).

- c. Several approaches had been taken by different manufacturers in complying with the noted regulations. If dynamic effects due to rigid body modes or airframe flexibility during taxi were not considered critical, some manufacturers used a simplified static analysis where a static inertia force was applied to the airplane using a load factor of 2.0 for single axle gears or 1.7 for multiple axle gears. The lower 1.7 factor was justified based on an assumption that there was a load alleviating effect resulting from rotation of the beam, on which the forward and aft axles are attached, about the central pivot point on the strut. The static load factor approach was believed to encompass any dynamic effects and it had the benefit of a relatively simple analysis.
- d. As computers became more powerful and dynamic analysis methods became more sophisticated, it was found that dynamic effects sometimes resulted in loads greater than those which were predicted by the static criterion. Some manufacturers performed calculations using a series of harmonic bumps to represent a runway surface, tuning the bumps to excite various portions of the structure at a given speed. U.S. Military Standard 8862 defines amplitude and wavelengths of 1-cosine bumps intended to excite low speed plunge, pitch and wing first bending modes.
- e. Some manufacturers used actual runway profile data to calculate loads. The runway profiles of the San Francisco Runway 28R or Anchorage Runway 24, which were known to cause high loads on airplanes and were the subject of pilot complaints until resurfaced, have been used in a series of bi-directional constant speed analytical runs to determine loads. In some cases, accelerated runs have been used, starting from several points along the runway. The profiles of those runways are described in NASA Reports CR-119 and TN D-5703. Such deterministic dynamic analyses have in general proved to be satisfactory.
- f. Some manufacturers have used a statistical power spectral density (PSD) approach, especially to calculate fatigue loads. Extensive PSD runway roughness data exist for numerous world runways. The PSD approach is not considered practical for calculation of limit loads due to difficulties in simulating the non-linearities in the landing gear shock absorption features.
- g. Because the various methods described above produce different results, the guidance information given in paragraphs 4, 5, and 6 of this AC should be used when demonstrating compliance with § 25.491.

4. <u>RUNWAY PROFILE CONDITION</u>.

a. Consideration of airframe flexibility and landing gear dynamic characteristics is necessary in most cases. A deterministic dynamic analysis, based on the San Francisco Runway 28R (before it was resurfaced), described in Table 1 of this AC, is an acceptable method for compliance.

- b. Airplane design loads should be developed for the most critical conditions arising from taxi, takeoff, and landing run. The airplane analysis model should include significant airplane rigid body and flexible modes, and the appropriate landing gear and tire characteristics. Unless the airplane has design features that would result in significant asymmetric loads, only the symmetric cases need be investigated.
- c. Airplane steady aerodynamic effects should normally be included. However, they may be ignored if their deletion is shown to produce conservative loads. Unsteady aerodynamic effects on dynamic response may be neglected.
- d. Conditions should be run at the maximum takeoff weight and the maximum landing weight with critical combinations of wing fuel, payload, and extremes of center of gravity (c.g.) range. For airplanes with trimable stabilizers, the stabilizer should be set within the appropriate green band setting for takeoff cases and at the recommended final approach setting for landing cases. The elevator should be assumed faired throughout the takeoff or landing run, unless other normal procedures are specified in the flight manual.
- e. A series of constant speed runs should be made in both directions from 20 knots up to the maximum ground speeds expected in normal operation (VR for takeoff conditions, 1.25 VL2 for landing conditions). Using only accelerated runs is not recommended due to the possibility that the speed/roughness points which could produce peak dynamic loads could be missed. For maximum take-off weight cases, the analysis should account for normal takeoff flap and control settings and consider both zero and maximum thrust. For maximum landing weight cases, the analysis should account for normal flap and spoiler positions following landing, and steady pitching moments equivalent to those produced by braking with a coefficient of friction of 0.3 with and without reverse thrust. The effects of automatic braking systems that reduce braking in the presence of reverse thrust may be taken into account.
- 5. <u>DISCRETE LOAD CONDITION</u>. One of the following discrete limit load conditions should be evaluated:
- a. With all landing gears in contact with the ground, the condition of a vertical load equal to 1.7 times the static ground reaction should be investigated under the most adverse airplane loading distribution at maximum takeoff weight, with and without thrust from the engines;
- b. As an alternative to paragraph 5(a) above, it would be acceptable to undertake dynamic analyses under the same conditions considered in paragraph 4 of this AC considering the aircraft response to each of the following pairs of identical and contiguous 1-cosine upwards bumps on an otherwise smooth runway:
- (i) Bump wavelengths equal to the mean longitudinal distance between nose and main landing gears, or between the main and tail landing gears, as appropriate; and separately.
 - (ii) Bump wavelengths equal to twice this distance.

The bump height in each case should be defined as:

$$H = 1.2 + 0.023 \sqrt{L}$$

Where--

H = the bump height (inches).

L = the bump wavelength (inches)

- 6. <u>COMBINED LOAD CONDITION</u>. A condition of combined vertical, side and drag loads should be investigated for the main landing gear. In the absence of a more rational analysis a vertical load equal to 90% of the ground reaction from paragraph 5 above should be combined with a drag and side load of 20% of the vertical load.
- 7. <u>TIRE CONDITIONS</u>. The calculation of maximum gear loads in accordance with paragraphs 4, 5, and 6, may be performed using fully inflated tires. For multiple wheel units, the maximum gear loads should be distributed between the wheels in accordance with the criteria of § 25.511.

TABLE 1

SAN FRANCISCO RUNWAY 28R

ONE TRACK

LENGTH: 3880 FEET

NUMBER OF POINTS: 1941 POINT SPACING: 2 FEET ELEVATIONS: FEET

REFERENCE SOURCE: REPORT TO NASA (EFFECTS OF RUNWAY UNEVENNESS ON THE DYNAMIC RESPONSE OF SUPERSONIC TRANSPORTS), JULY 1964, U. OF

CALIF. BERKLEY.

RUNWA	Y ELEV	ATION P	OINTS II	N FEET (READ R	ow wis:	E):
10.300	10.310	10.300	10.300	10.310	10.320	10.330	10.340
10.350	10.360	10.360	10.370	10.370	10.370	10.380	10.390
10.400	10.400	10.410	10.410	10.420	10.430	10.430	10.440
10.440	10.440	10.440	10.440	10.450	10.460	10.470	10.470
10.480	10.490	10.490	10.500	10.500	10.500	10.500	10.500
10.500	10.490	10.490	10.490	10.490	10.500	10.500	10.510
10.510	10.520	10.520	10.520	10.530	10.530	10.540	10.540
10.550	10.550	10.550	10.550	10.540	10.550	10.550	10.560
10.570	10.570	10.570	10.570	10.570	10.580	10.570	10.570
10.580	10.570	10.560	10.560	10.560	10.560	10.560	10.560
10.560	10.560	10.550	10.550	10.550	10.560	10.570	10.570
10.570	10.570	10.560	10.550	10.550	10.550	10.550	10.550
10.560	10.560	10.560	10.560	10.550	10.540	10.530	10.520
10.520	10.520	10.520	10.520	10.520	10.530	10.520	10.520
10.510	10.520	10.520	10.510	10.520	10.520	10.530	10.530
10.530	10.530	10.530	10.530	10.530	10.530	10.530	10.520
10.530	10.540	10.540	10.540	10.540	10.540	10.540	10.550
10.550	10. 540	10.550	10.550	10.560	10.570	10.580	10.590
10.600	10.610	10.620	10.630	10.650	10.6 60	10.660	10.670
10.660	10.670	10.670	10.670	10.670	10.670	10.660	10.660
10.650	10.650	10.650	10.650	10.660	10.670	10.670	10.670
10.6 80	10.680	10.680	10.690	10.690	10. 690	10.700	10.710
10.710	10.720	10.720	10.710	10.720	10.720	10.720	10.710
10.720	10.720	10.730	10.730	10.740	10.750	10.750	10.780
10.770	10.780	10.790	10.800	10.810	10.810	10.820	10.830
10.840	10.850	10.860	10.860	10.860	10.860	10.850	10.860
10.860	10.870	10.870	10.870	10.870	10.870	10.860	10.850
10.840	10.840	10.830	10.830	10.840	10.850	10.860	10.870
10.870	10.880	10.890	10.900	10.920	10.930	10.940	10.950

10.950	10.950	10.950	10.950	10.950	10.960	10.970	10.980
10.980	10.990	10.990	10.990	11.000	11.010	11.010	11.010
11.010	10.980	10.960	10.950	10.950	10.950	10.960	10.970
10.970	10.980	10.970	10.970	10.980	10.990	11.000	11.010
11.030	11.030	11.030	11.030	11.030	11.030	11.030	11.010
11.020	11.020	11.030	11.040	11.050	11.050	11.040	11.060
11.070	11.070	11.080	11.080	11.090	11.100	11.120	11.130
11.140	11.140	11.150	11.160	11.170	11.170	11.170	11.170
11.170	11.180	11.180	11.180	11.170	11.170	11.170	11.170
11.190	11.170	11.180	11.180	11.180	11.190	11.190	11.190
11.200	11.210	11.210	11.210	11.200	11.200	11.200	11.190
11.180	11.180	11.170	11.160	11.150	11.140	11.140	11.140
11.120	11.110	11.090	11.090	11.090	11.090	11.090	11.090
11.090	11.090	11.090	11.090	11.090	11.090	11.090	11.080
11.080	11.080	11.080	11.070	11.060	11.050	11.040	11.030
11.020	11.010	11.000	10.990	10.990	10.9 80	10.990	10.980
10.980	10.980	10.980	10.980	10.980	10.9 90	10.9 90	11.000
11.000	11.000	11.000	11.000	11.010	11.020	11.020	11.020
11.020	11.020	11.020	11.010	11.010	11.000	11.000	11.000
11.000	11.000	11.000	10.990	10.990	10.980	10.9 90	10.990
11.000	11.010	11.010	11.010	11.030	11.040	11.030	11.050
11.060	11.070	11.060	11.070	11.080	11.080	11.080	11.090
11.090	11.080	11.080	11.080	11.080	11.080	11.080	11.070
11.080	11.080	11.080	11.080	11.090	11.080	11.080	11.070
11.070	11.060	11.050	11.050	11.040	11.050	11.040	11.040
11.040	11.040	11.040	11.040	11.040	11.030	11.030	11.030
11.030	11.020	11.020	11.020	11.020	11.020	11.020	11.030
11.030	11.040	11.050	11.050	11.060	11.060	11.060	11.070
11.070	11.070	11.070	11.070	11.080	11.080	11.070	11.070
11.070	11.060	11.060	11.060	11.060	11.060	11.070	11.070
11.080 11.090	11.080	11.090	11.090	11.090	11.090	11.100	11.090
11.070	11.090 11.090	11.090	11.080	11.080	11.070	11.070	11.060
11.120	11.110	11.100 11.110	11.100	11.110	11.110	11.120	11.120
11.120	11.110		11.110	11.110	11.110	11.100	11.110
11.110	11.120	11.120 11.100	11.120 11.100	11.110 11.120	11.110	11.120	11.110
11.170	11.110	11.180	11.100	11.120	11.130	11.150	11.160
11.230	11.230	11.230	11.190	11.190	11.200 11.250	11.220	11.220
11.230	11.230	11.230	11.240	11.230	11.230	11.260	11.240

1	1.270	11.280	11.280	11.300	11.310	11.320	11.330	11.340
1	1.340	11.340	11.340	11.330	11.320	11.320	11.310	11.320
1	1.320	11.310	11.310	11.310	11.320	11.310	11.320	11.330
.1	1.340	11.350	11.350	11.360	11.360	11.360	11.370	11.370
1	1.370	11.370	11.380	11.380	11.380	11.380	11.380	11.380
1	1.380	11.380	11.380	11.370	11.370	11.370	11.370	11.380
1	1.380	11.390	11.380	11.380	11.390	11.400	11.410	11.410
1	1.420	11.430	11.440	11.440	11.450	11.460	11.460	11.460
1	1.460	11.470	11.480	11.480	11.480	11.490	11.500	11.500
1	1.500	11.500	11.500	11.500	11.490	11.490	11.490	11.480
1	1.470	11.460	11.460	11.480	11.460	11.470	11.470	11.470
. 1	1.470	11.460	11.450	11.450	11.450	11.460	11.460	11.460
1	1.450	11.450	11.450	11.450	11.450	11.460	11.460	11.460
1	1.480	11.470	11.470	11.480	11.480	11.480	11.480	11.490
· 1	1.490	11.500	11.510	11.520	$11.5\overline{20}$	11.520	11.520	11.520
1	1.520	11.520	11.530	11.520	11.520	11.520	11.530	11.530
1	1.530	11.530	11.530	11.530	11.540	11.530	11.520	11.520
1	1.510	11.530	11.520	11.540	11.530	11.540	11.530	11.540
	1.530	11.540	11.550	11.540	11.540	11.540	11.540	11.530
	1.520	11.510	11.500	11.490	11.490	11.490	11.490	11.490
	1.480	11.470	11.470	11.470	11.460	11.470	11.470	11.480
	1.470	11.460	11.460	11.460	11.460	11.460	11.470	11.470
	1.470	11.460	11.460	11.440	11.430	11.410	11.400	11.390
	1.380	11.370	11.360	11.360	11.350	11.350	11.350	11.350
	1.350	11.340	11.340	11.330	11.320	11.320	11.320	11.310
	1.310	11.300	11.290	11.290	11.280	11.280	11.280	11.280
	1.280	11.270	11.270	11.270	11.260	11.260	11.250	11.250
	1.240	11.230	11.220	11.210	11.190	11.180	11.170	11.170
	1.150	11.130	11.120	11.100	11.100	11.180	11.170	11.140
	1.140	11.120	11.000	10.970	10.950	10.940	10.920	10.910
	0.920	10.920	10.910	10.930	10.930	10.930	10.930	10.930
	0.930	10.930	10.930	10.930	10.930	10.930	10.940	10.940
	0.940	10.940	10.950	10.940	10.930	10.940	10.940	10.930
	0.920	10.920	10.920	10.910	10.910	10.910	10.910	10.900
	0.890	10.880	10.870	10.890	10.880	10.880	10.880	10.870
	0.860	10.850	10.860	10.860	10.850	10.850	10.850	10.840
	0.840	10.840	10.830	10.830	10.820	10.820	10.810	10.810
1	0.800	10.790	10.790	10.790	10.790	10.790	10.790	10.800

10.800	10.810	10.820	10.820	10.830	10.840	10.850	10.850
10.850	10.870	10. 870	10.880	10.870	10.880	10.870	10.870
10.870	10.870	10.860	10.850	10.840	10. 840	10.840	10.840
10.840	10.830	10.820	10.820	10.820	10.820	10.820	10.820
10.830	10.820	10.830	10.820	10.820	10.820	10.820	10.810
10.810	10.810	10.810	10.820	10.820	10.820	10.830	10.830
10.830	10.840	10.840	10.850	10.860	10.860	10.860	10.880
10.870	10.860	10.860	10.860	10.870	10.870	10.860	10.850
10.850	10.890	10.910	: 10.910	10.920	10.920	10.930	10.930
10.930	10.940	10.940	10.950	10.940	10.930	10.930	10.920
10.930	10.910	10.910	10.900	10.900	10.900	10.910	10.910
10.890	10.900	10.910	10.910	10.910	10.920	10.930	10.940
10.940	10.940	10.940	10.940	10.950	10.930	10.930	10.930
10.930	10.920	10.930	10.930	10.930	10.930	10.910	10.900
10.910	10.910	10.910	10.910	10.910	10.910	10.910	10.900
10.900	10.890	10.900	10.900	10.900	10.910	10.900	10.910
10.890	10.890	10. 890	10.890	10. 890	10. 880	10.8 80	10.870
10.870	10.870	10.860	10.880	10.870	10.860	10.870	10.870
10.860	10.850	10.850	10.850	10.860	10.850	10.860	10.860
10.860	10.870	10.870	10.870	10.870	10.870	10.880	10.870
10.880	10.870	10.880	10.880	10.880	10.880	10.880	10.890
10.900	10.890	10.890	10.890	10.890	10.900	10.890	10.890
10.880	10.870	10.880	10.870	10.870	10.870	10.870	10.880
10.880	10.880	10.880	10.880	10.880	10.890	10.890	10.890
10.890	10.890	10.890	10.890	10.880	10.880	10.890	10.880
10.890	10.880	10.880	10.880	10.880	10.880	10.870	10.870
10.870	10.870	10.870	10.880	10.880	10.880	10.890	10.890
10.900	10.910	10.920	10.920	10.930	10.920	10.920	10.920
10.920	10.920	10.920	10.920	10.930	10.930	10.930	10.930
10.930	10.940	10.930	10.930	10.930	10.930	10.930	10.920
10.920	10.910	10.900	10.920	10.910	10.910	10.900	10.900
10.900	10.880	10.880	10.860	10.850	10.850	10.840	10.840
10.840	10.840	10.850	10.850	10.850	10.850	10.850	10.850
10.860 10.910	10.860	10.860	10.870	10.880	10.880	10.890	10.900
10.910	10.910	10.920	10.920	10.930	10.940	10.940	10.950
11.000	10.960	10.970	10.990	10.990	10.990	10.990	11.000
	11.000	11.010	11.010	11.020	11.020	11.020	11.040
11.05 0	11.050	11.060	11.060	11.050	11.040	11.030	11.030

11.020	11.020	11.020	11.040	11.060	11.040			
11.020	11.030	11.030	11.040	11.050	11.060	11.070	11.090	
11.100	11.100	11.110	11.120	11.140	11.140	11.150	11.160	
11.160	11.160	11.150	11.150	11.160	11.150	11.140	11.140	
11.140	11.140	11.140	11.140	11.150	11.150	11.150	11.150	
11.150	11.150	11.160	11.160	11.150	11.150	11.160	11.160	
11.160	11.160	11.160	11.160	11.160	11.160	11.170	11.170	
11.170	11.170	11.170	11.170	11.170	11.160	11.150	11.150	
11.140	11.140	11.140	11.130	11.120	11.120	11.120	11.120	
11.120	11.120	11.130	11.130	11.140	11.150	11.160	11.170	
11.180	11.190	11.200	11.200	11.220	11.230	11.240	11.240	
11.250	11.260	11.270	11.280	11.280	11.290	11.300	11.300	
11.300	11.310	11.300	11.310	11.310	11.310	11.310	11.300	
11.300	11.300	11.290	11.290	11.290	11.290	11.290	11.290	
11.290	11.290	11.290	11.300	11.300	11.310	11.310	11.320	
11.320	11.330	11.330	11.340	11.350	11.350	11.350	11.350	
11.350	11.350	11.360	11.360	11.350	11.350	11.350	11.350	
11.350	11.350	11.340	11.340	11.340	11.340	11.350	11.350	
11.350	11.340	11.330	11.330	11.330	11.330	11.330	11.330	
11.330	11.320	11.330	11.330	11.330	11.330	11.330	11.340	
11.340	11.340	11.350	11.350	11.350	11.350	11.350	11.350	
11.350	11.350	11.360	11.360	11.360	11.350	11.350	11.350	
11.350	11.350	11.350	11.360	11.360	11.360	11.360	11.360	
11.370	11.380	11.380	11.390	11.390	11.400	11.410	11.420	
11.420	11.430	11.430	11.420	11.420	11.430	11.430	11.430	
11.430	11.430	11.430	11.440	11.440	11.450	11.460	11.460	
11.470	11.480	11.480	11.490	11.490	11.500	11.500	11.510	
11.520	11.520	11.520	11.520	11.520	11.520	11.520	11.520	
11.520	11.520	11.510	11.510	11.510	11.500	11.500	11.500	
11.500	11.510	11.510	11.510	11.520	11.520	11.520	11.520	
11.530	11.530	11.530	11.520	11.520	11.520	11.520	11.520	
11.520	11.530	11.530	11.530	11.540	11.530	11.530	11.540	
11.540	11.540	11.540	11.530	11.530	11.530	11.530	11.540	
11.540	11.540	11.550	11.550	11.550	11.560	11.550	11.550	
11.550	11.550	11.540	11.530	11.530	11.530	11.510	11.520	
11.520	11.530	11.530	11.540	11.550	11.560	11.560	11.570	
11.570	11.570	11.580	11.580	11.580	11.580	11.580	11.580	
11.590	11.590	11.590	11.590	11.580	11.570	11.570	11.580	
11.570	11.570	11.570	11.580	11.580	11.590	11.600	11.620	

11.610	11.610	11.610	11.610	11.610	11.620	11.630	11.640
11.650	11.660	11.670	11.670	11.670	11.680	11.700	11.720
11.730	11.740	11.760	11.770	11.780	11.800	11.820	11.820
11.820	11.830	11.820	11.820	11.830	11.840	11.830	11.830
11.830	11.830	11.830	11.830	11.840	11.850	11.860	11.870
11.880	11.880	11.890	11.900	11.900	11.900	11.900	11.900
11.900	11.910	11.910	11.900	11.910	11.910	11.910	11.910
11.900	11.910	11.910	11.920	11.920	11.920	11.920	11.920
11.920	11.920	11.910	11.910	11.920	11.910	11.910	11.910
11.910	11.900	11.900	11.900	11.900	11.900	11.900	11.900
11.900	11.900	11.900	11.910	11.920	11.920	11.920	11.930
11.930	11.930	11.930	11.940	11.940	11.950	11.950	11.950
11.960	11.960	11.960	11.960	11.960	11.960	11.950	11.940
11.930	11.920	11.920	11.920	11.920	11.920	11.920	11.920
11.920	11.920	11.920	11.920	11.910	11.900	11.900	11.900
11.900	11.900	11.900	11.900	11.900	11.900	11.900	11.900
11.900	11.900	11.900	11.900	11.900	11.890	11.880	11.880
11.870	11.870	11.860	11.860	11.850	11.850	11.840	11.840
11.840	11.840	11.840	11.850	11.870	11.890	11.890	11.900
11.890	11.920	11.950	11.950	11.950	11.940	11.940	11.930
11.920	11.920	11.910	11.900	11.900	11.890	11.880	11.870
11.860	11.850	11.840	11.840	11.840	11.830	11.820	11.820
11.810	11.830	11.830	11.830	11.840	11.840	11.840	11.840
11.820	11.830	11.820	11.830	11.830	11.840	11.840	11.840
11.850	11.840	11.840	11.840	11.850	11.850	11.850	11.860
11.860	11.840	11.840	11.840	11.840	11.840	11.840	11.840
11.840	11.840	11.840	11.840	11.840	11.830	11.830	11.830
11.820	11.830 11.830	11.830 11.840	11.830 11.840	11.820	11.820	11.830	11.820
11.830	11.840	11.840	11.840	11.830	11.830	11.830	11.830
11.840	11.840	11.850	11.850	11.850 11.860	11.850 11.860	11.850 11.870	11.850
11.870	11.870	11.870	11.860	11.870	11.870	11.880	11.870 11.890
11.890	11.890	11.910	11.910	11.920	11.930	11.950	11.950
11.960	11.960	11.960	11.960	11.920	11.960	11.960	11.960
11.960	11.950	11.950	11.940	11.960	11.980	11.990	12.010
12.030	12.040	12.050	12.050	12.050	12.050	12.050·	12.010
12.040	12.060	12.060	12.070	12.070	12.070	12.070	12.060
12.070	12.070	12.080	12.080	12.080	12.090	12.090	12.080
	· ·						

12.080	12.080	12.080	12.080	12.090	12.100	12.100	12 100
12.100	12.100	12.110	12.110	12.120	12.130	12.130	12.100
12.130	12.140	12.140	12.130	12.130	12.130	12.110	12.130
12.070	12.060	12.070	12.080	12.090	12.100		12.100
12.120	12.060	12.010	12.030	12.040	12.100	12.110	12.110
12.060	12.050	12.040	12.030	12.020	12.030	12.050	12.060
12.010	11.990	11.980	11.940	11.940		12.020	12.020
11.910	11.900	11.900	11.900		11.930	11.930	11.920
11.880	11.870	11.870	11.860	11.900	11.900	11.910	11.900
11.850	11.850	11.850		11.860	11.850	11.860	11.860
11.850	11.840		11.860	11.860	11.870	11.860	11.860
11.880		11.850	11.850	11.870	11.890	11.880	11.880
	11.890	11.900	11.910	11.910	11.910	11.910	11.920
11.920	11.930	11.940	11.940	11.950	11.950	11.950	11.950
11.950	11.960	11.950	11.950	11.960	11.970	11.980	11.980
11.990	12.000	12.000	11.990	11.990	11.990	12.000	12.000
12.010	12.020	12.020	12.030	12.040	12.050	12.060	12.060
12.060	12.060	12.060	12.060	12.060	12.060	12.070	12.080
12.090	12.100	12.090	12.120	12.130	12.140	12.130	12.140
12.140	12.140	12.150	12.150	12.160	12.160	12.170	12.170
12.170	12.150	12.140	12.130	12.120	12.110	12.100	12.090
12.090	12.090	12.080	12.070	12.070	12.060	12.050	12.030
12.030	12.020	12.010	12.020	12.010	12.010	12.010	12.010
12.020	12.020	12.010	12.000	12.000	11.980	11.970	11.970
11.960	11.960	11.960	11.960	11.950			,

Note: The National Aeronautics and Space Administration (NASA) Report CR-119 identifies an elevation of 10.97 inches at 1620 feet. This is considered a typographical error and has been corrected in this table. The elevation is 10.87 inches.

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revised 12-16-97: JT editorial changes

revised 7-22-98: Incorporates ANM-7 changes (no directorate comments were

incorporated)